

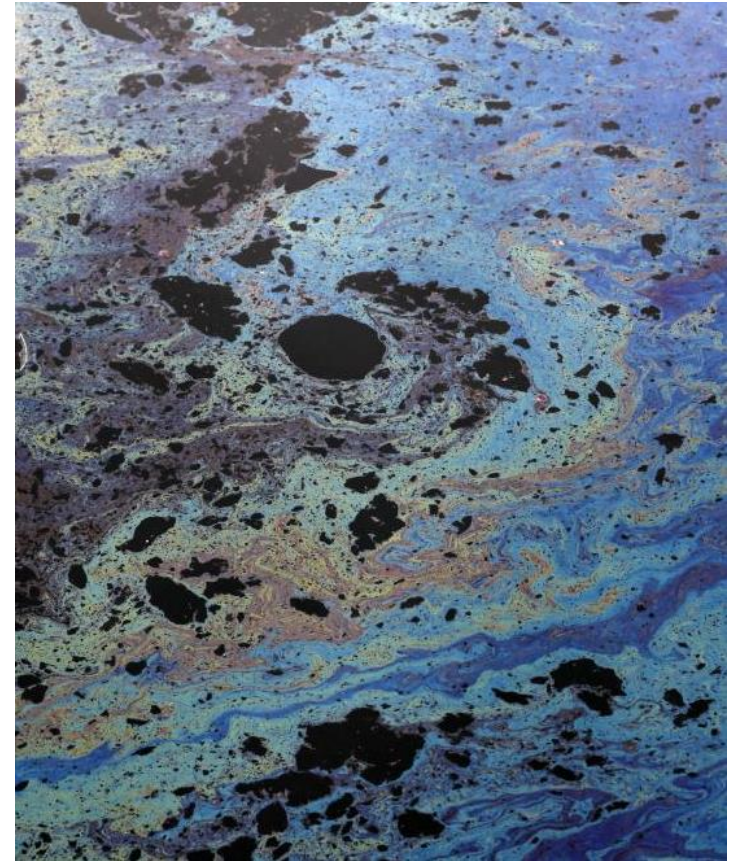
# Effect of surface contamination on isotropic-turbulence-driven interfacial gas transfer

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# Background

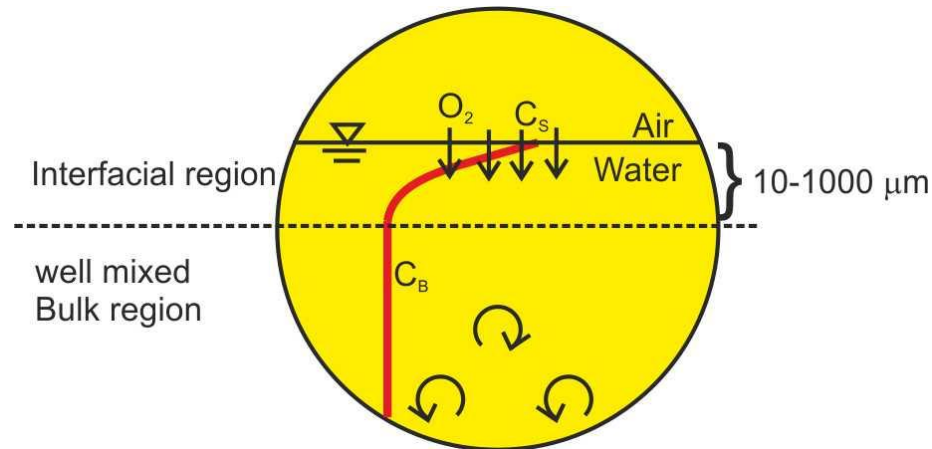
# Interfacial Mass Transfer

Gas transfer ; molecular diffusion ↔ turbulence in the water phase

Advective-diffusive :  $\langle j_z \rangle = - \left[ D \frac{\partial \langle c \rangle}{\partial z} - \langle w' c' \rangle \right]$

j: gas flux  
D: molecular diffusion  
c: concentration  
w: vertical velocity

Gas transfer of low-diffusive gases ( $O_2$ ,  $CO_2$ ) is marked by a very thin concentration boundary layer at the water side



# Pollution

**Focus is on interfacial pollution by surfactants**

**Surfactants reduce the surface stress of water**

**Surface divergence typically leads to non-uniform surfactant concentrations**

**Which is counteracted by the Marangoni effect trying to force surface divergence to zero.**

# Modelling Pollution Effects

Surface tension,  $\sigma$ , depends on the pollutant concentration,  $\gamma$ .

$$\sigma = \sigma(\gamma)$$

After normalization define the Marangoni number by

$$Ma = - \frac{d\sigma}{d\gamma}$$

which we assume to be constant. From the model presented in Shen *et al.*, (2004) JFM, Vol. 506, after some algebra, we obtain:

$$\left. \frac{\partial u}{\partial z} \right|_{interface} = - \frac{Ma Re}{We} \frac{\partial \gamma}{\partial x}$$

$$\left. \frac{\partial v}{\partial z} \right|_{interface} = - \frac{Ma Re}{We} \frac{\partial \gamma}{\partial y}$$

$u$ : x-velocity

$v$ : y-velocity

$Re$ : Reynolds number

$We$ : Weber number

$\gamma$ : surfactant concentr.

# Aim

To determine a parametrization of the effect of pollution on the interfacial gas transfer velocity  $K_L$

For a clean (no pollution) interface  $K_L$  scales as

$$K_L \propto Sc^{-1/2}$$

where  $Sc$  is the Schmidt number.

For a very dirty interface

$$K_L \propto Sc^{-2/3}$$

What happens at (very) moderate levels of pollution?

$$K_L \propto Sc^{-q}$$

The power  $q$  will likely depend on  $\frac{Ma Re}{We}$

# Problem Investigated

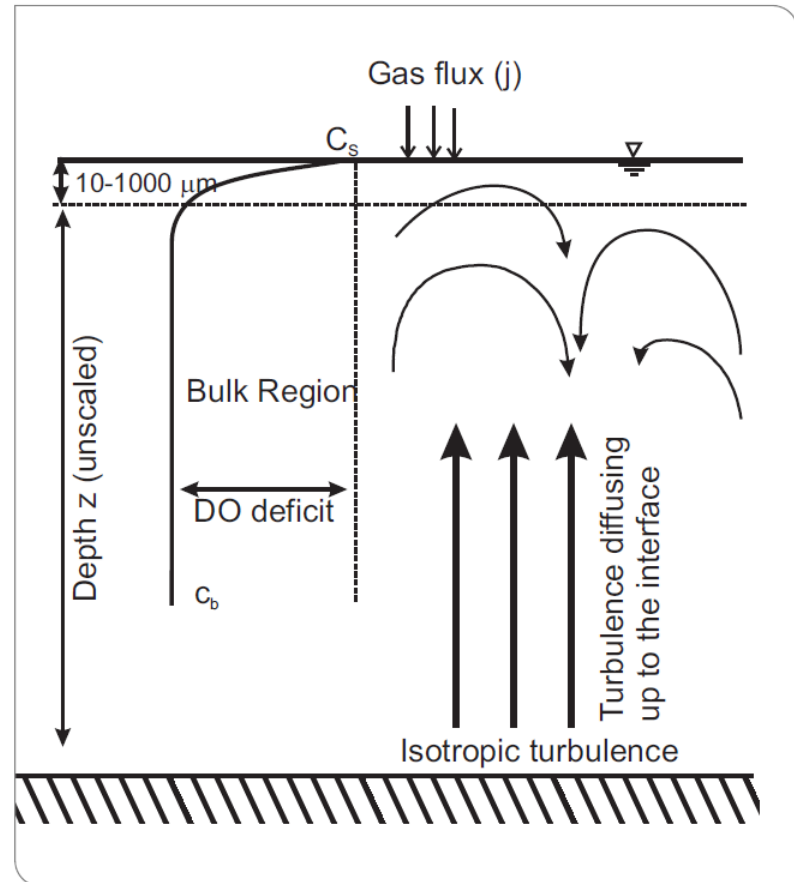
# Physical Problem

## Grid-stirred-driven gas transfer

Convenient analogy to bottom shear induced turbulence



[www.xs4all/rdemming/travel/Indonesia](http://www.xs4all/rdemming/travel/Indonesia)





# Computational Setup

## Boundary conditions

$$\text{Top: } \left. \frac{\partial u_i}{\partial z} \right|_{top} = - \frac{Ma Re}{We} \frac{\partial \gamma}{\partial x_i}, i = 1, 2$$

$x_1, u_1$ : x, x-velocity  
 $x_2, u_2$ : y, y-velocity

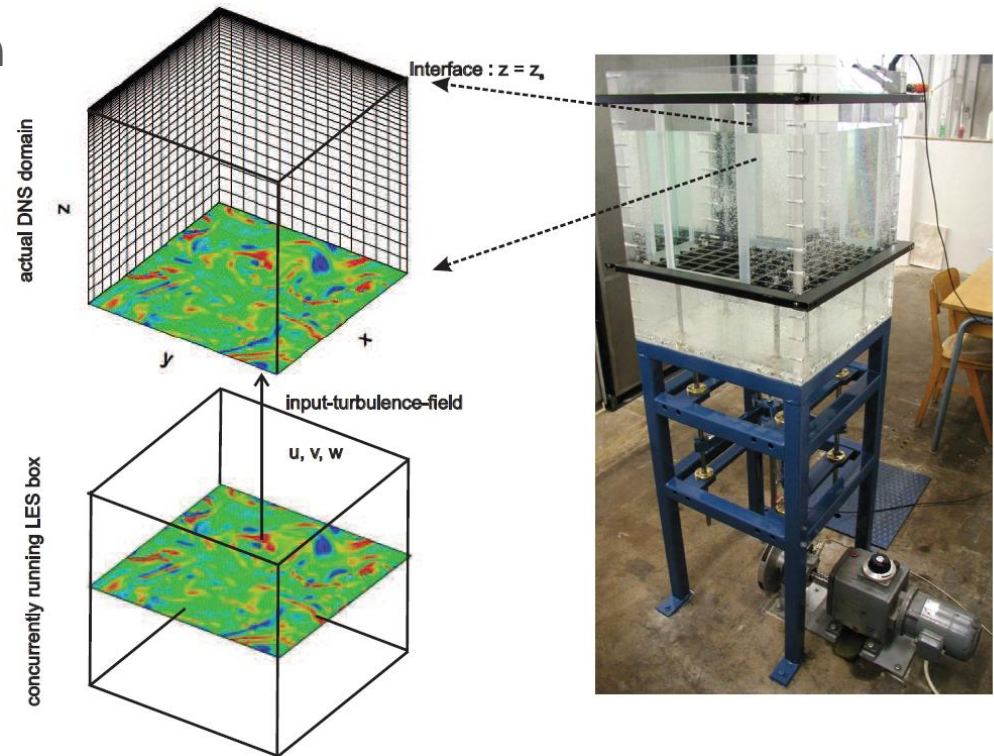
various levels of contamination

Sides: periodic

Bottom: flow-field copied from isobox

$c_{top} = 1$   
(saturated at all times)

$$c_{bottom} \rightarrow \frac{\partial c}{\partial z} = 0$$



# Simulations performed

Simulation	Re Ma/We
S30p0	30
S6p0	6
S1p2	1.2
S0p6	0.6
S0p12	0.12

**For all DNS simulations:**

**128 x 128 x 212 mesh for the box of size 5L x 5L x 3L**

**Mesh is refined in the z-direction towards the surface**

**Surfactant Schmidt number = 2**

**Turbulent flow with  $Tu = 40\%$  introduced at the bottom**

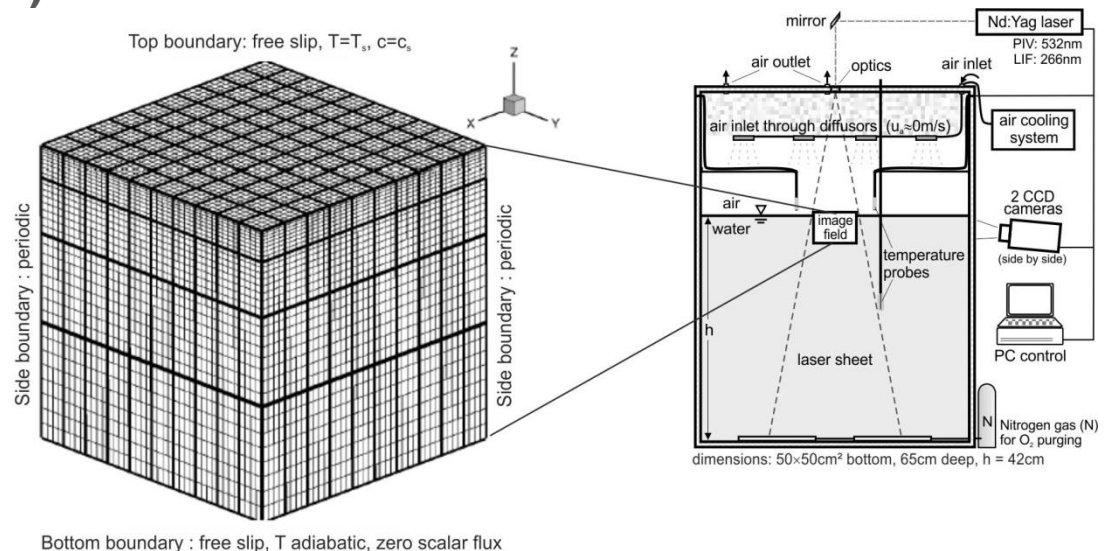
# Numerical Method

Flow fields in main DNS and LES isobox are solved using fourth-order discretisations of convection and diffusion.

A dual mesh strategy is used where up to five scalars can be solved simultaneously on a refined mesh

A fifth-order-accurate WENO scheme is used for scalar convection, combined with a fourth order central discretisation for scalar diffusion (same in 2D for surfactant).

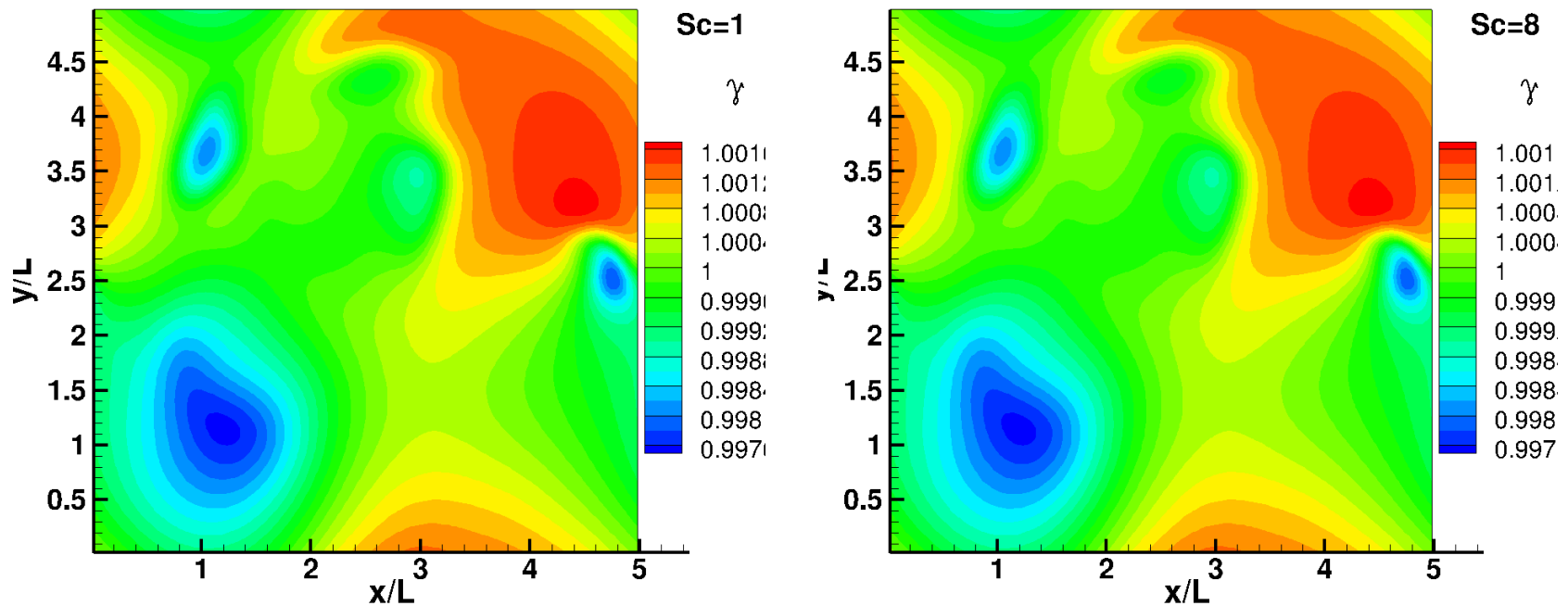
Standard Message passing interface (MPI) is applied for communication between blocks.



# Surfactant Diffusivity

# How important is Surfactant Diffusivity?

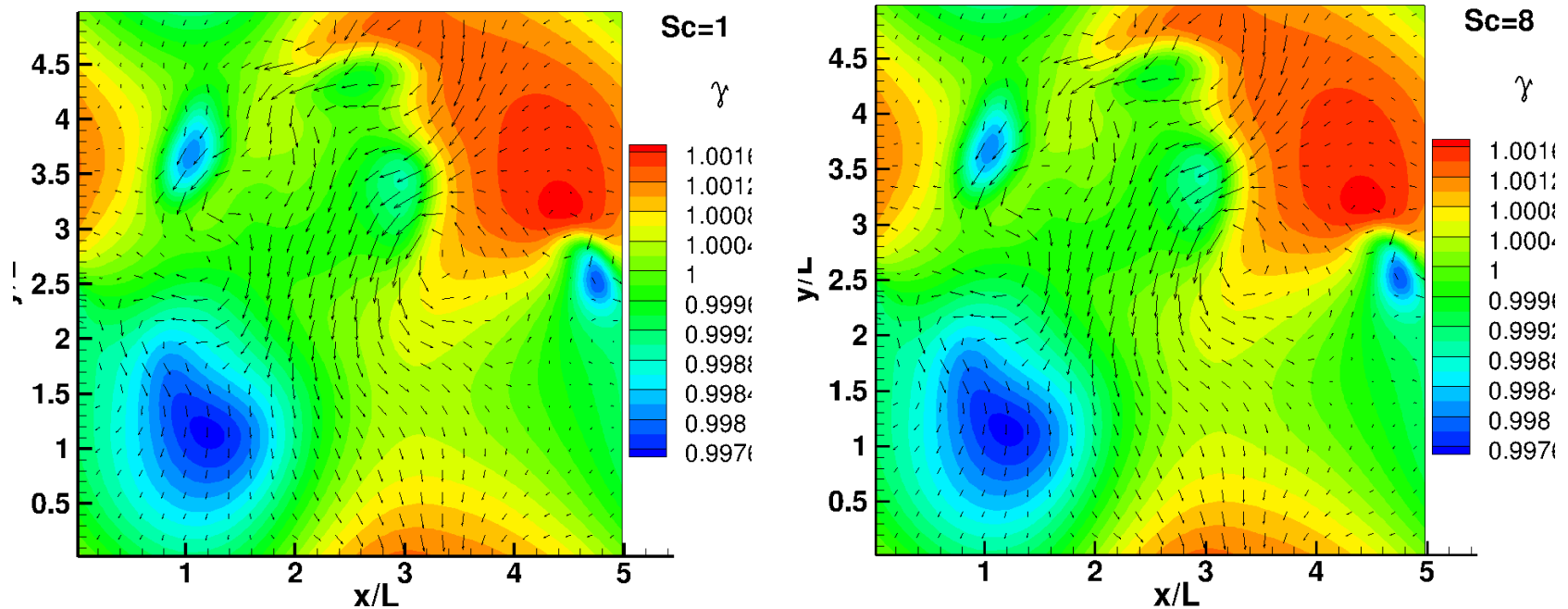
Surfactant distribution for various  $Sc = \frac{\nu}{D_{surf}}$



Snapshots of  $\gamma$  at  $t = 100 L/U$

# How important is Surfactant Diffusivity?

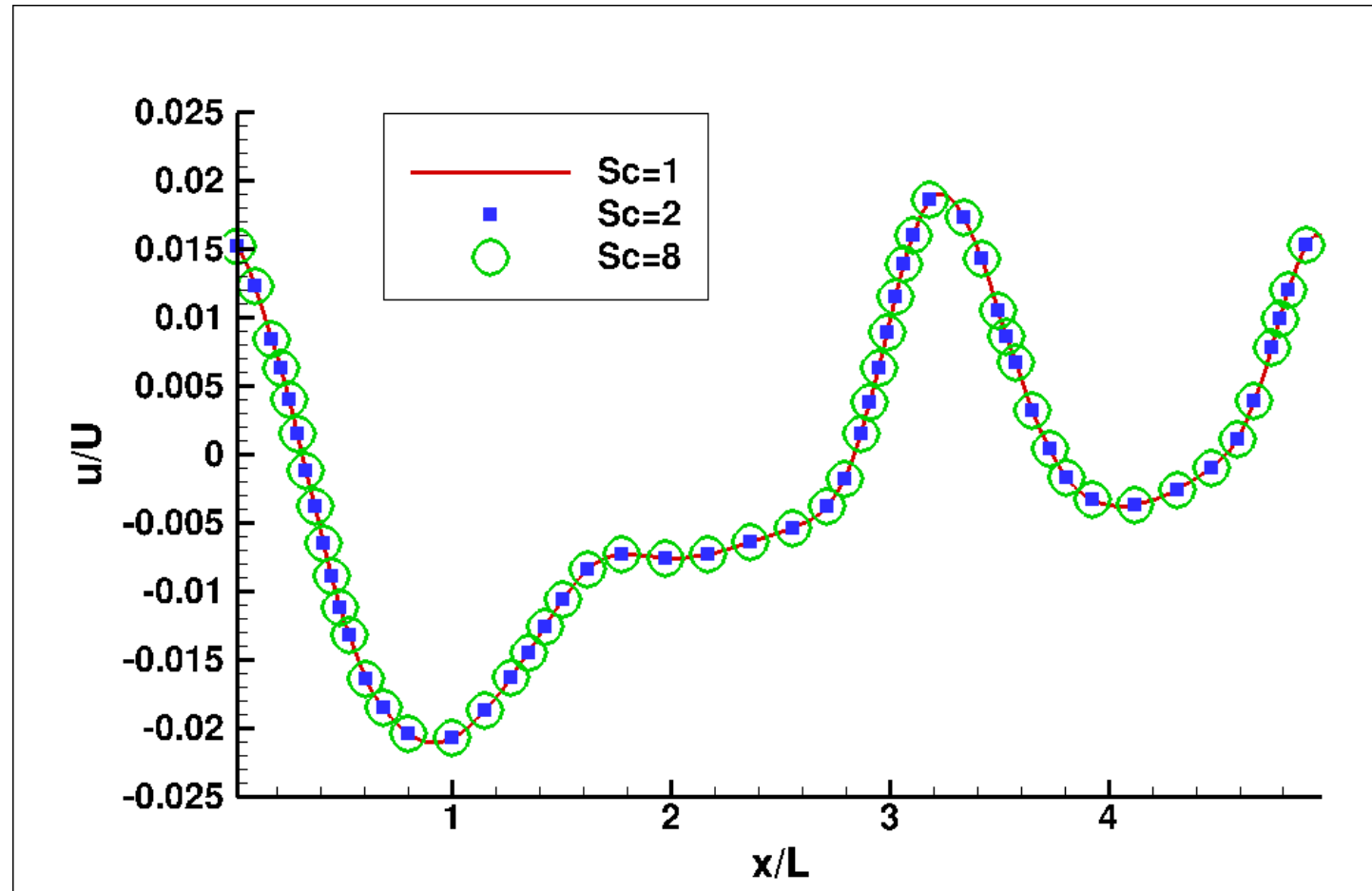
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Snapshots of  $\gamma$  at  $t = 100 L/U$

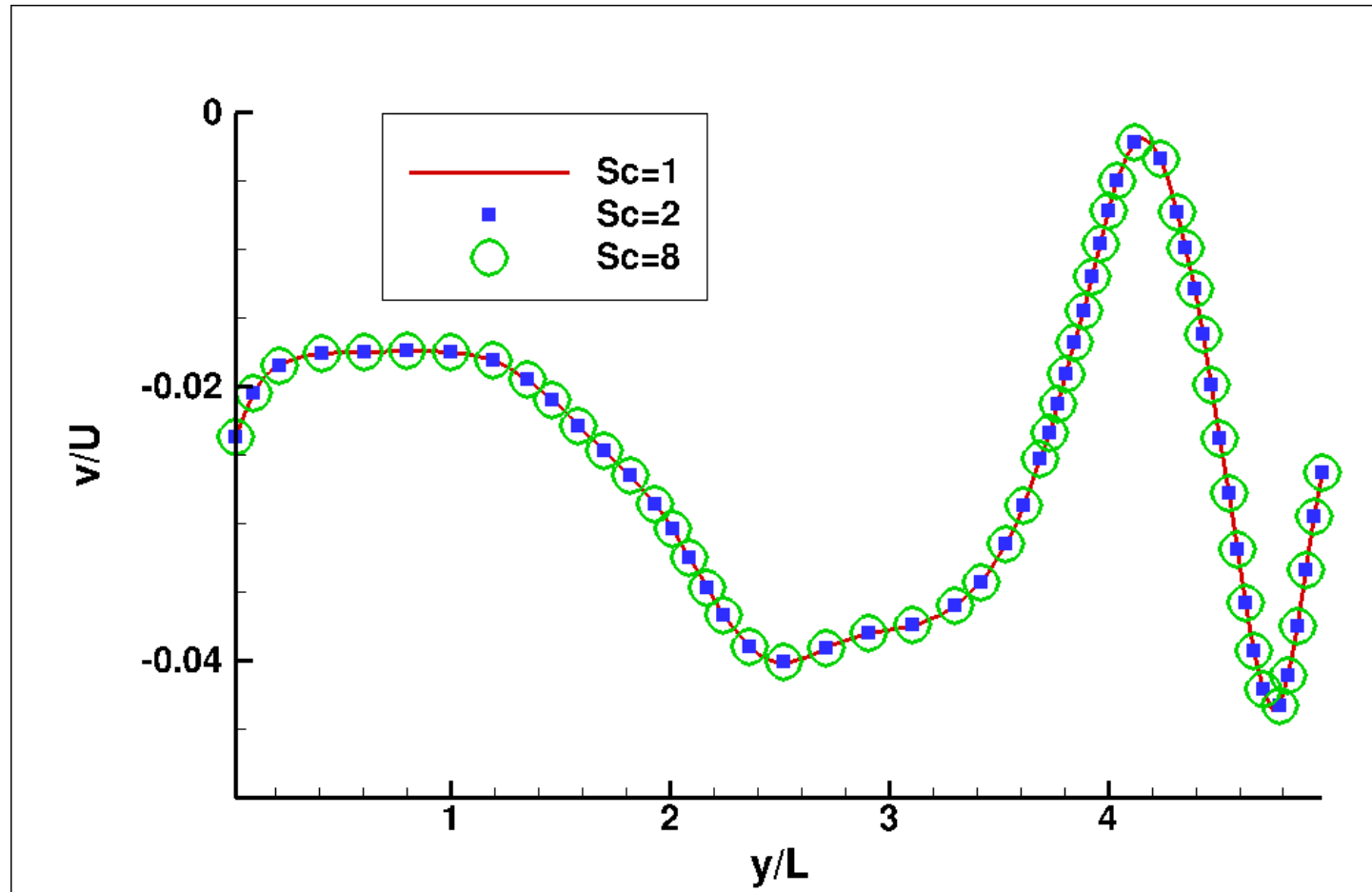
# How important is Surfactant Diffusivity?

Effect on interfacial u-velocity at  $y/L = 2.5$



# How important is Surfactant Diffusivity?

Effect on interfacial v-velocity at  $x/L = 2.5$

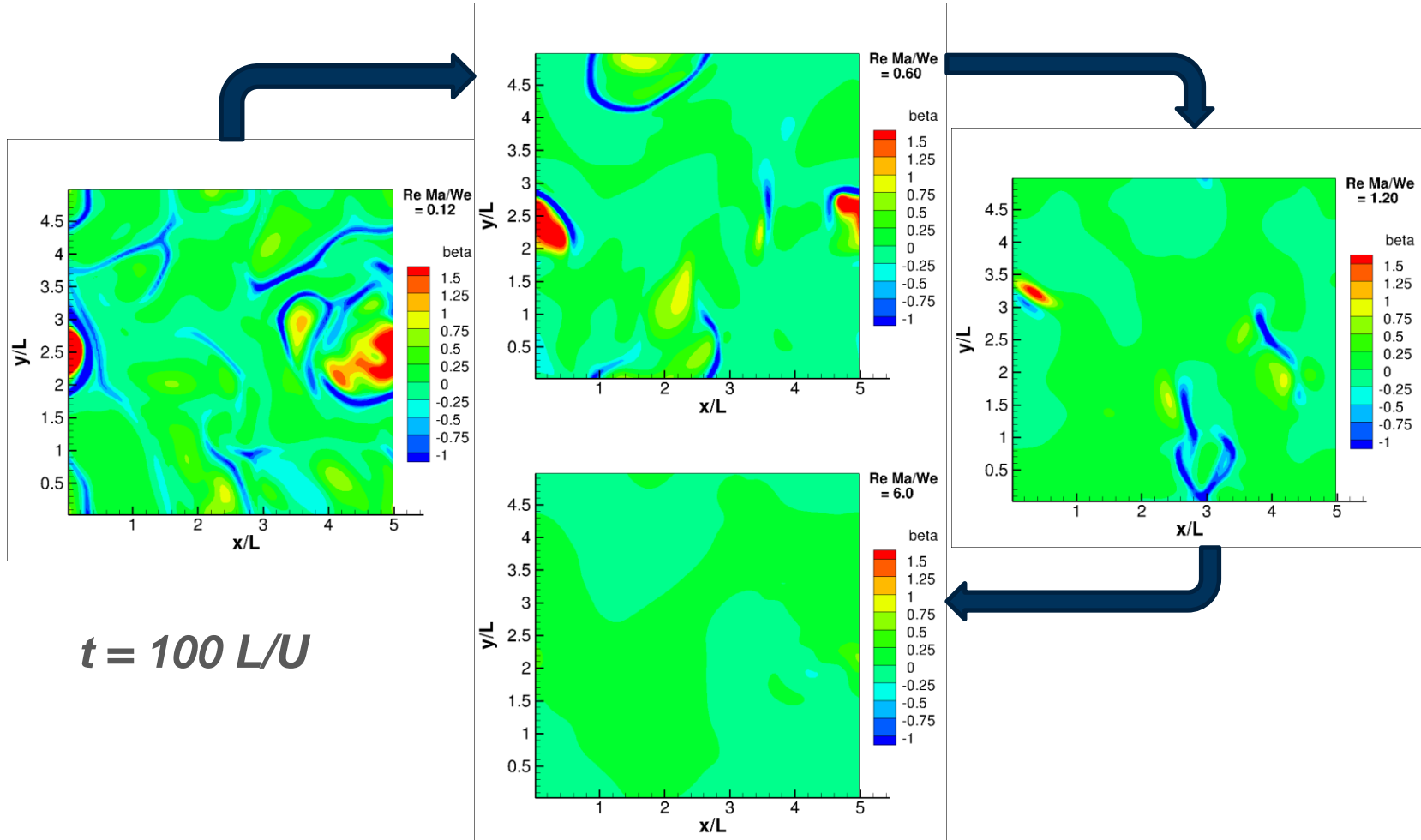




# Preliminary Results

# Surface Divergence $\beta$

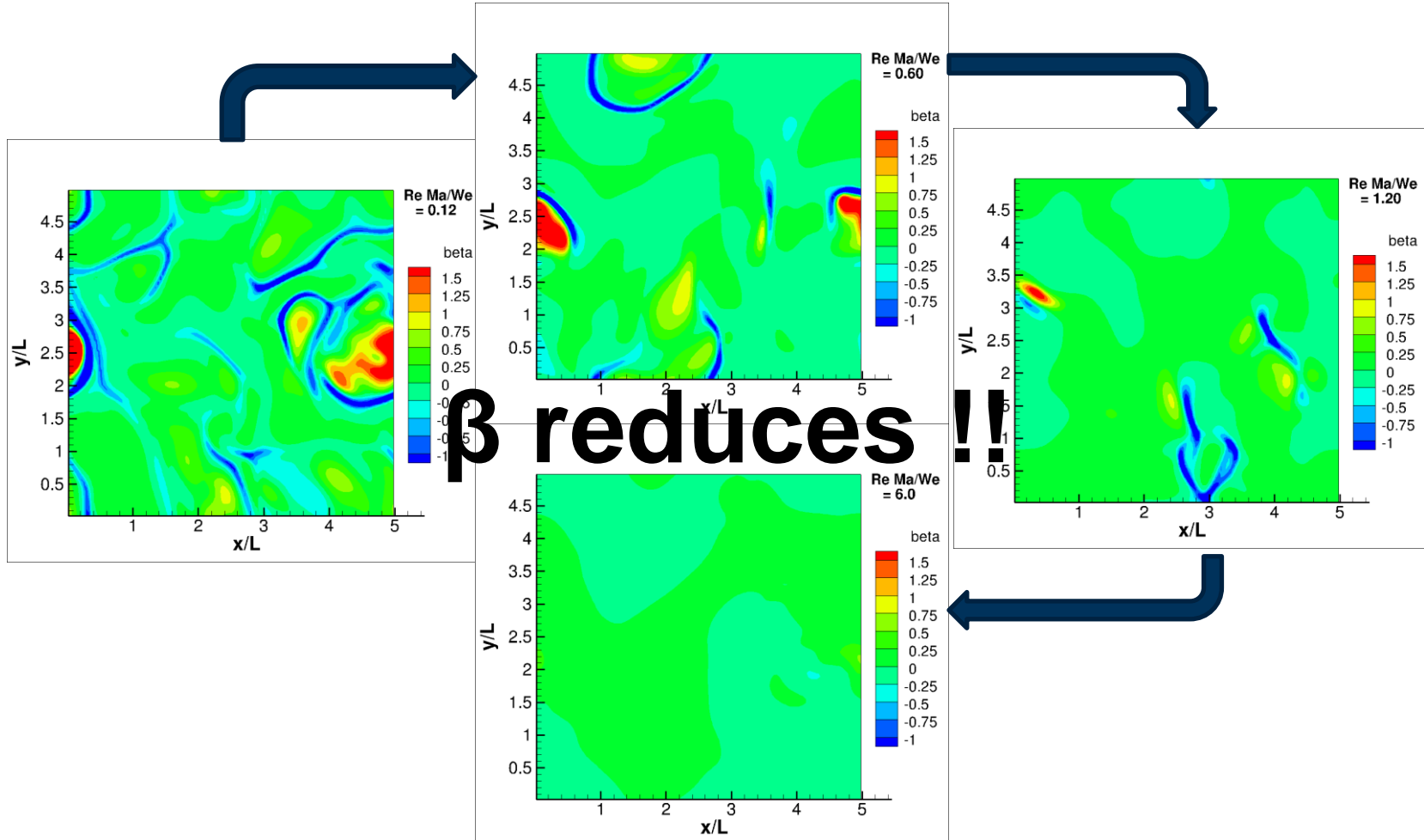
Effect of increasing  $Re\ Ma/We$



$t = 100 L/U$

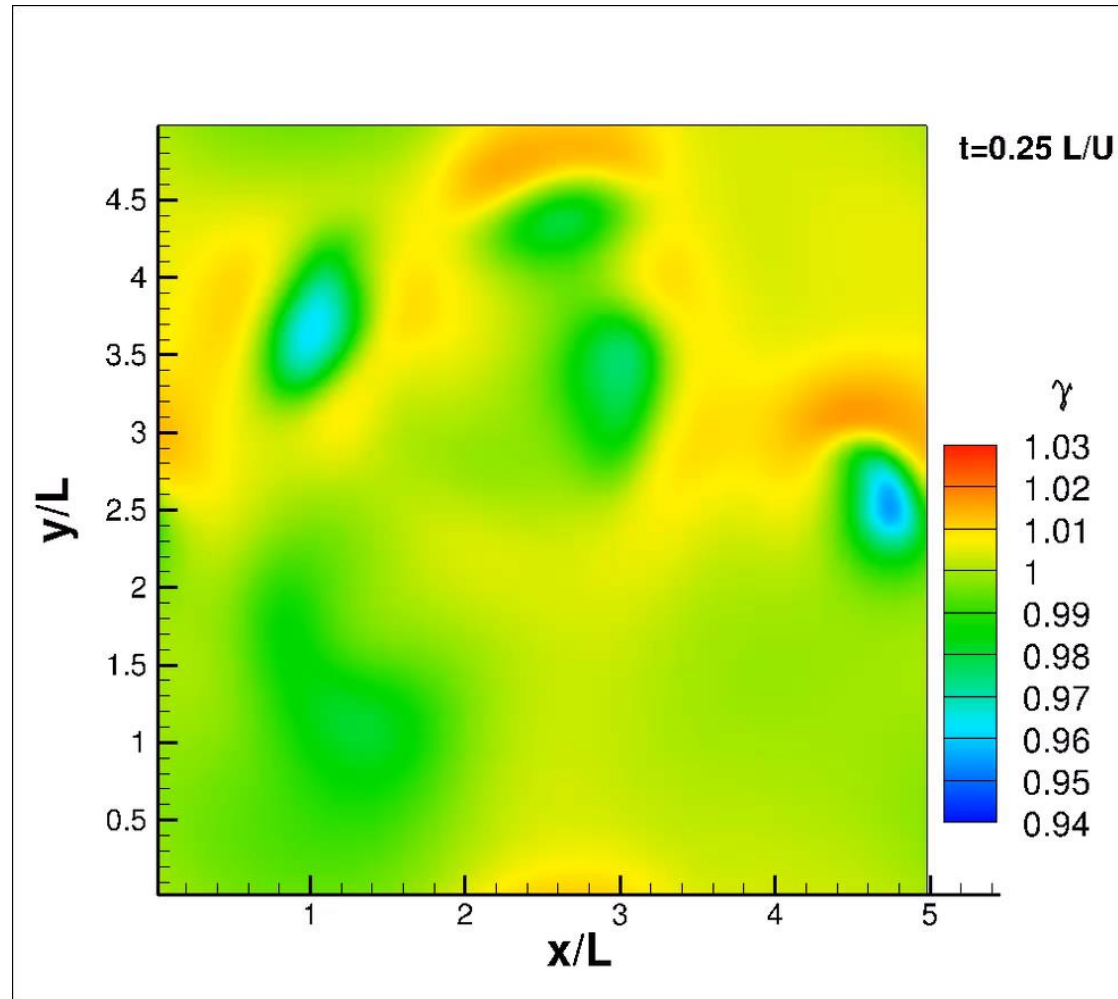
# Surface Divergence $\beta$

Effect of increasing  $Re\ Ma/We$



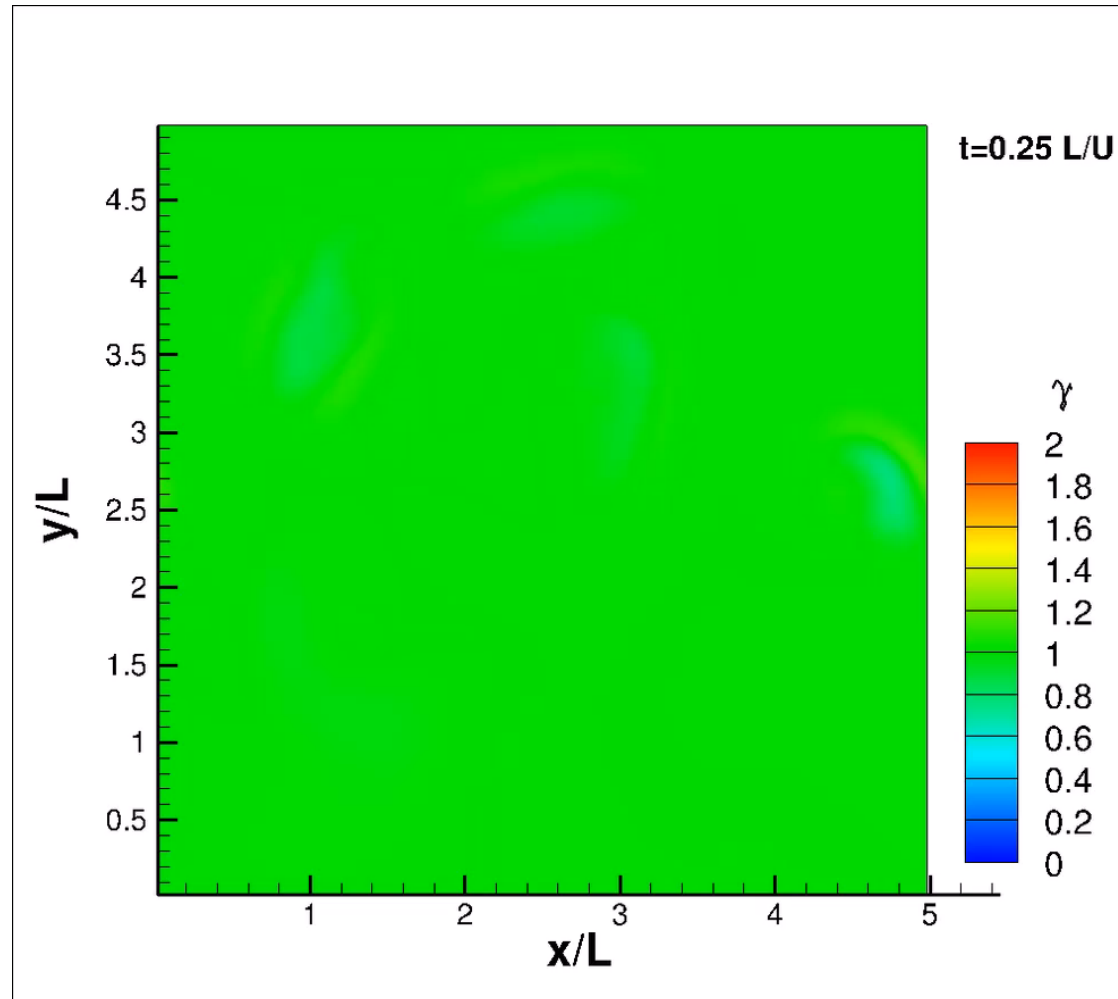
# Surfactant Concentration Distribution

$$Re\ Ma/We = 30.0$$



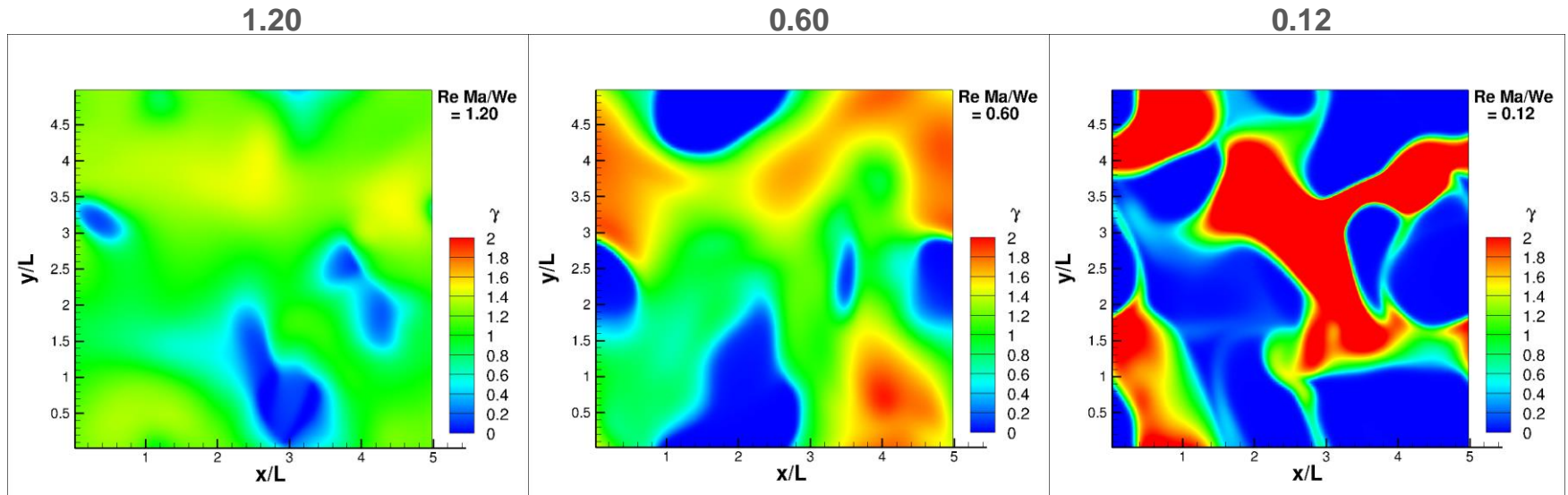
# Surfactant Concentration Distribution

$$Re\ Ma/We = 0.12$$



# Surfactant Concentration Distribution

## Effect of decreasing $Re\ Ma/We$



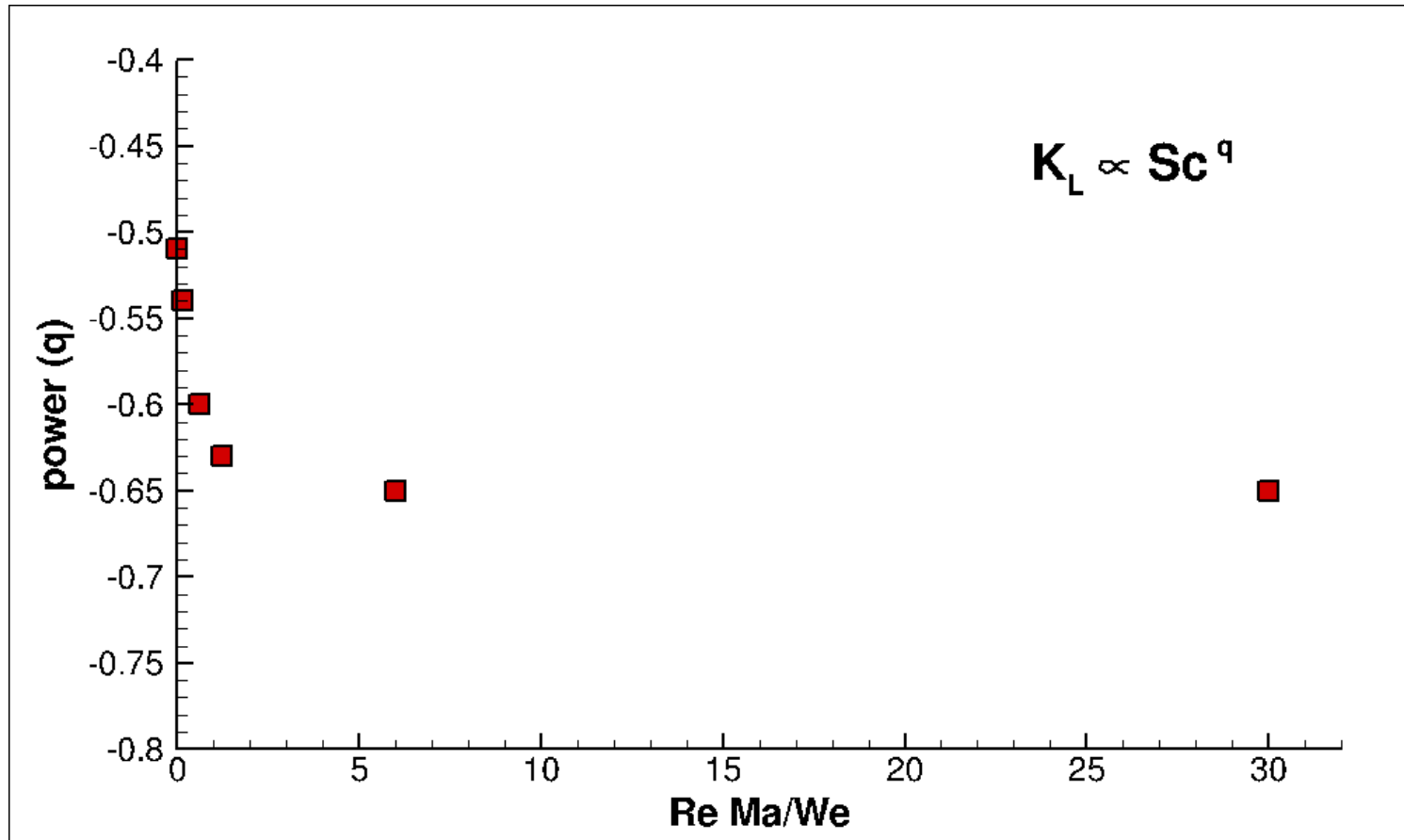
With decreasing  $Re\ Ma/We$  clean surface regions grow in size

In these regions  $K_L$  will scale with  $Sc^{-1/2}$

In the remaining regions  $K_L$  may scale with  $Sc^{-2/3}$  ???

# Transfer Velocity Scaling

Effect of increasing  $Re\ Ma/We$

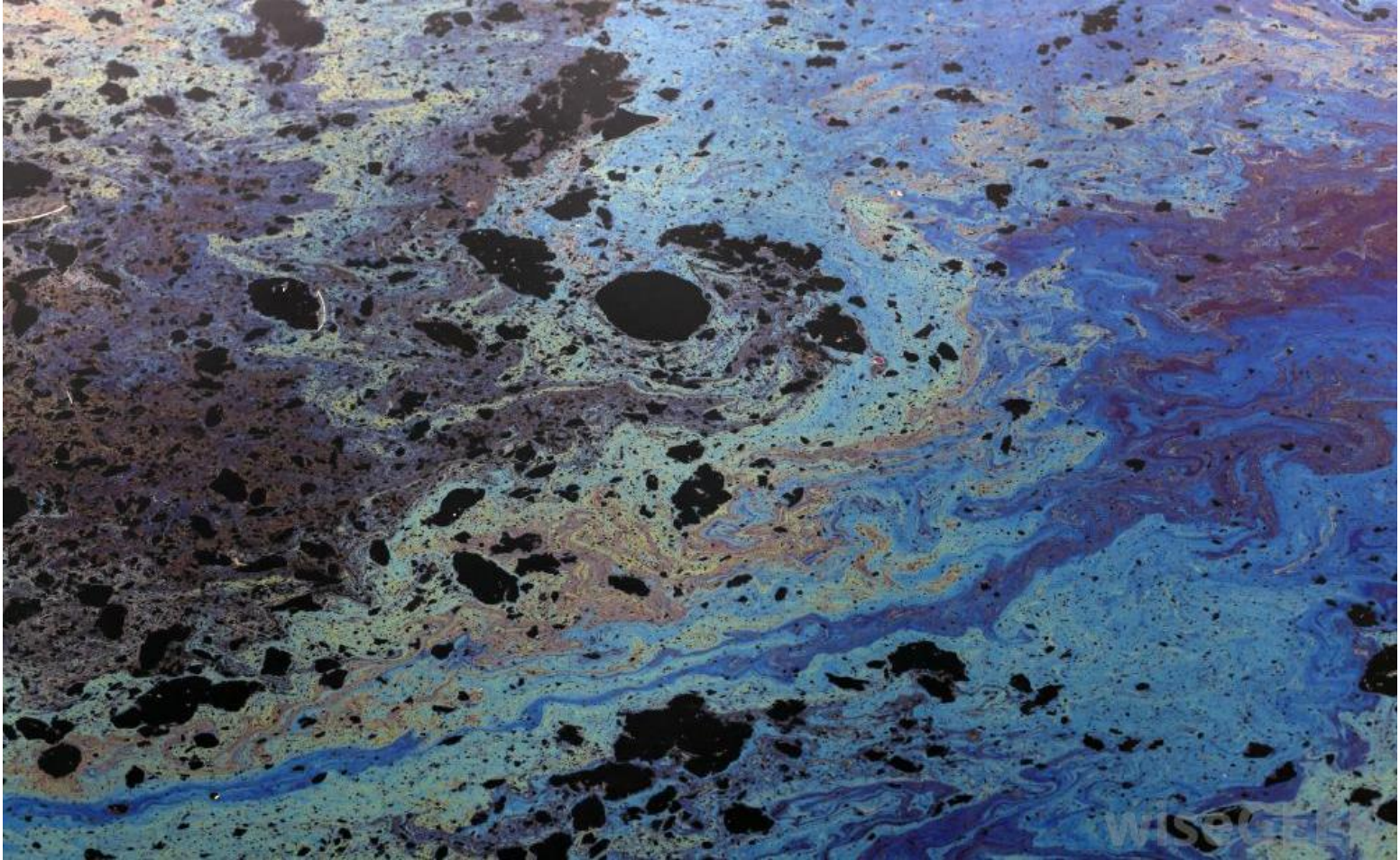


# Conclusions

- It was confirmed that the surfactant transport is largely unaffected by the amount of diffusivity
- Even low levels of contaminations can have a large effect on interfacial gas flux
- With increasing  $Re\ Ma/We$ , the surface divergence,  $\beta$ , becomes progressively damped
- Resulting in a quick transition to a  $K_L \propto Sc^{-2/3}$  scaling which is typical for a no-slip surface (shear!!)
- At lower  $Re\ Ma/We$  areas on the surface will develop with a zero surfactant concentration



# The end



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